

Fermilab

TM-967
1650

CENTRAL: A COMPUTER PROGRAM TO DO PERFORMANCE CALCULATIONS FOR A HELIUM LIQUEFIER

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ABSTRACT

The flow diagram for a helium liquefier is shown in Figure 1. The computer program described here thoroughly analyzes the operating cycle of the liquefier and predicts the values of the plant thermodynamic variables at all process points in the plant. The performance characteristics of the turboexpanders are calculated. The temperature distributions within the heat exchangers are checked for unphysical behavior. These calculations require 1.0 second of computer time and the results are immediately available in case real-time response is desired.

PROGRAM DESCRIPTION

The process points shown in Figure 1 are numbered to correspond to process instrumentation in the liquefier control room so that comparisons can be readily made without difficulty. The layout of the operators console is shown in Figure 2. Temperature, pressure and flow measurements are available to the operator of the plant. Enthalpy measurements are not made. No measure of turbine performance is available to the operator except for speed of rotation.

The heat exchangers are designated HX1 through HX8, beginning with the liquid nitrogen exchanger. These heat exchangers are grouped into four modules designated E16 through E19. Intermediate points within these modules are not instrumented although a complete analysis of the heat exchanger performance is performed by the program. The heat leak into each heat exchanger has been fully accounted for in the program at the correct temperature level.

The basis for the design of the plant is the TS diagram shown in Figure 3. A number is indicated in a circle for each process point on this diagram. The program supplies all the information shown on Figure 3 for any desired plant operating condition which is physically realizable.

The computer output is included in Figures 4 through 13. The program can be used interactively and contains initial set-point values to produce the operating conditions of Figures 3 and 4.

You should be aware that these calculations are made using several approximations which do not affect the results.

1. The pressure drop in the high-, medium- and low-pressure sides of the liquefier is introduced by summing discreet changes in pressure. Typical constant values for these changes have been included in the program.
2. The pressure PT17 is a parameter specified by the user. The value is used for the cold-end calculations regardless of the pressure in the low-pressure side.
3. In operation a total of approximately 1.0g/s of helium flows out of the process through the labyrinth seals of the turbo-expanders. The program neglects this flow which amounts to 0.07% of compressor discharge.
4. The program calculates the compressor work using an isothermal compression corrected by a compressor efficiency specified by the user.

PROGRAM VALIDATION

Naturally, some real-world test of the computer predictions is desirable. Because the performance of a liquefier of this type is highly constrained by the thermophysical properties of the process fluid, calculations of this type can be accurate and of value in identifying unphysical operating conditions. Program output for two known operating modes has been compared with the expected values.

First, the design TS diagram for the plant (Figure 3) is very closely reproduced by the program. The computed temperatures (Figure 4) agree to better than 0.1°K. This accuracy is good enough for operation of the liquefier. The mass flow predictions agree to a fraction of a percent.

The steady state characteristics of the heat exchangers are given in Figures 5 through 11. The minimum size of each heat exchanger has been calculated for the operating conditions corresponding to maximum liquefaction of the plant.

A second test of the program is shown in Figure 14. This TS diagram was computed by the program and corresponds to an entirely different operating mode of the plant; i.e., turbine T2 stopped. Information about this mode has been supplied by Sulzer and agrees with Figure 14 to about 1% of the helium flow. Notice that TT15 must be raised to operate HX7 and HX8. This requires the larger flow FT5 corresponding to the higher enthalpy at point 17.

SAMPLE RESULTS

The first sample of output from the program is Figure 15. This corresponds to making 4000 liters per hour with the plant while operating the compressors at the reduced discharge pressure of 125 psi. Notice that all of the temperatures on the low side

must be adjusted by approximately 1°K to produce the peak liquefaction. Nearly every heat exchanger is affected by these temperature changes. Liquid nitrogen flow is reduced 17% to control these temperatures. In addition, the flow through the turbines is increased by 8% above the nominal value.

A second sample is given in Figure 16 where the plant is being operated as an 8.0 kilowatt refrigerator. The work done by the turbines is greatly reduced. Otherwise, the temperatures in the plant were kept nearly unchanged by reducing liquid nitrogen consumption to 155g/s. Unchanged turbine efficiencies were assumed.

SUMMARY

The operating conditions predicted by the program CENTRAL are in good agreement with the currently available operating parameters for the liquefier. The program is a useful aid to study the performance of the liquefier and to analyze the operating conditions. The calculations are performed very rapidly so that instantaneous response is possible. The program could be used to train plant operators or as a diagnostic tool during plant operation. The program CENTRAL is approximately 2000 FORTRAN statements including comments.

FERMILAB

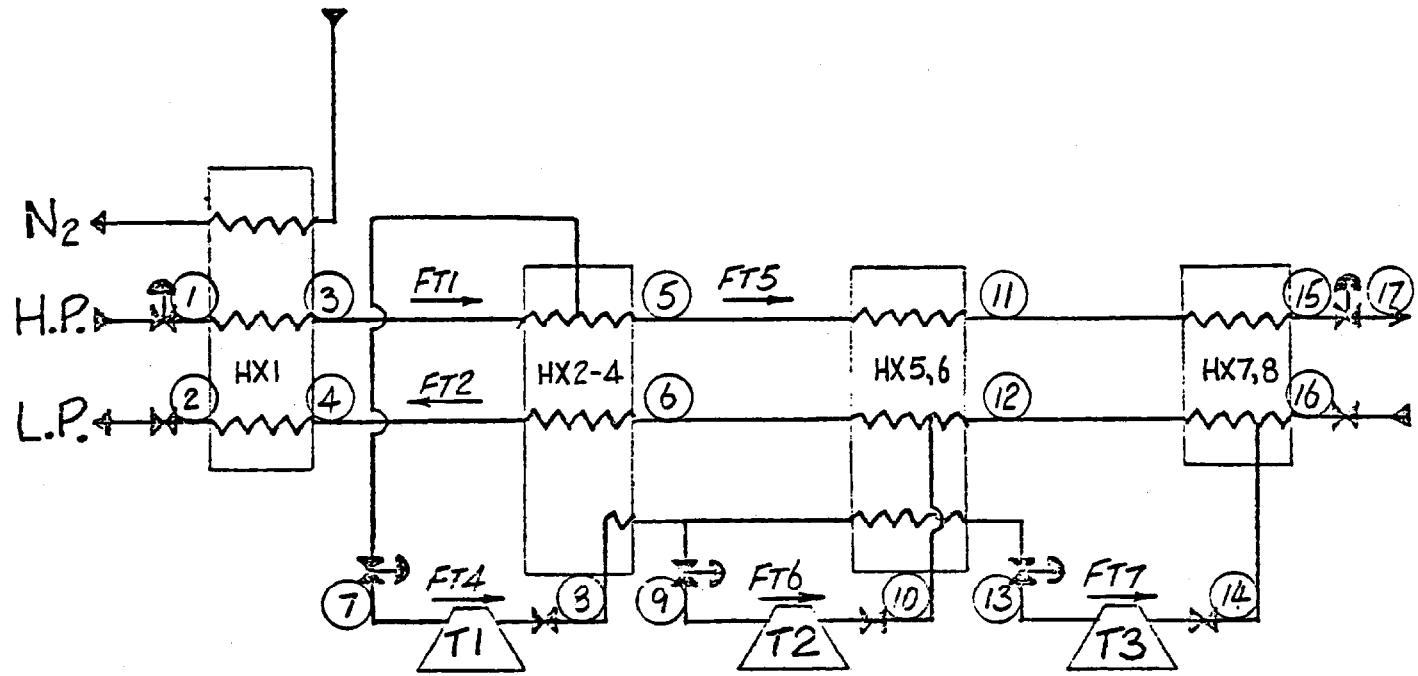
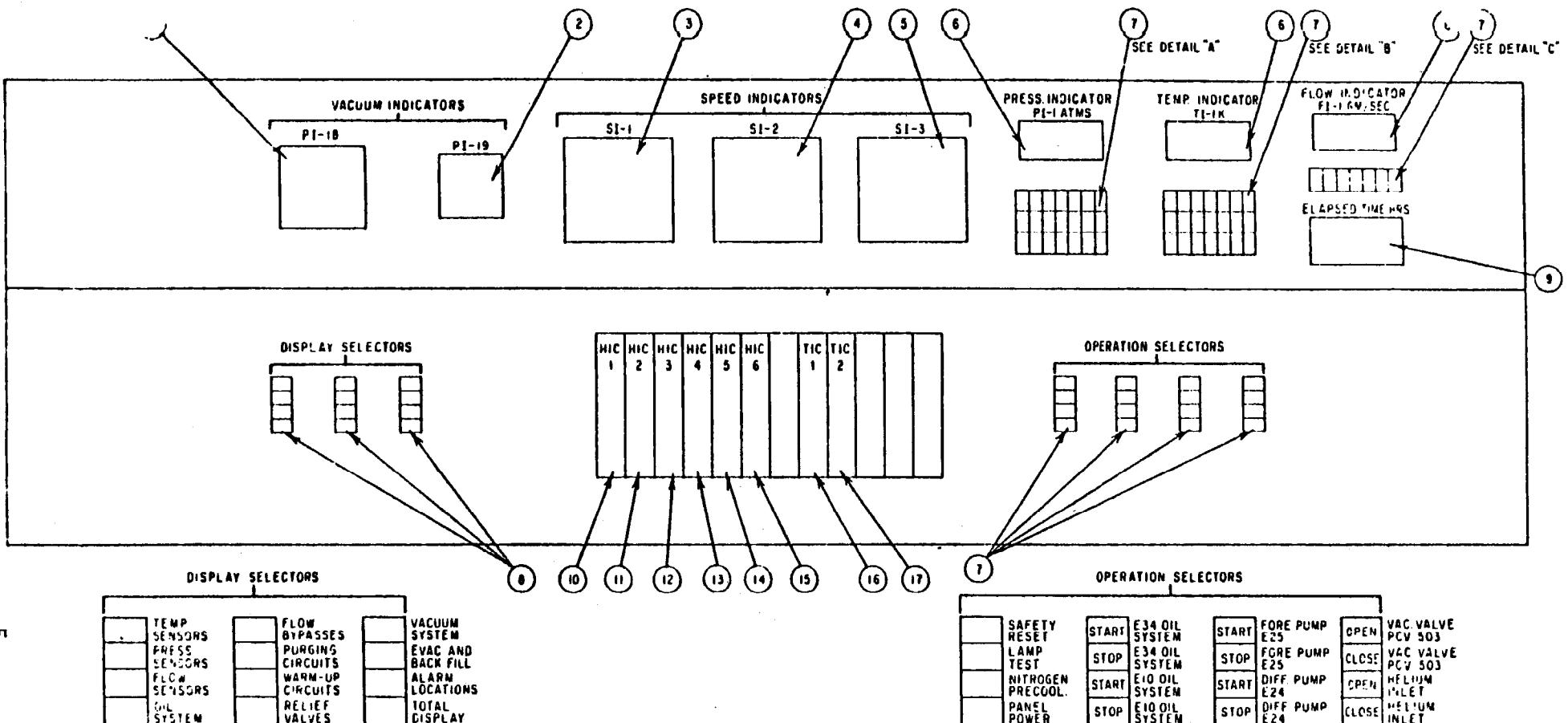


Figure 1.



ITEM NO	DESCRIPTION	DESIGNATION
1	COLD CATHODE ION GAUGE CONTROL	PI-18
2	I/C VACUUM GAUGE CONTROLLER	PI-19
3	SPEED INDICATOR	SI-1
4	SPEED INDICATOR	SI-2
5	SPEED INDICATOR	SI-3
6	DIGITAL METER	
7	SWITCHCRAFT SWITCH ASSEMBLY	
8	SWITCHCRAFT INDICATORS	
9	ELAPSED TIME (HOURS)	
10	HAND INDICATING CONTROLLER	HIC 1
11	HAND INDICATING CONTROLLER	HIC 2
12	HAND INDICATING CONTROLLER	HIC 3
13	HAND INDICATING CONTROLLER	HIC 4
14	HAND INDICATING CONTROLLER	HIC 5
15	HAND INDICATING CONTROLLER	HIC 6
16	TEMPERATURE INDICATING CONTROLLER	TIC 1
17	TEMPERATURE INDICATING CONTROLLER	TIC 2

| PT |
|----|----|----|----|----|----|----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| PT |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 |

DETAIL "A"

| TT |
|----|----|----|----|----|----|----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| TT |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 |

DETAIL "B"

FT	FT	FT	FT	FT	FT
1	2	3	4	5	6

DETAIL "C"

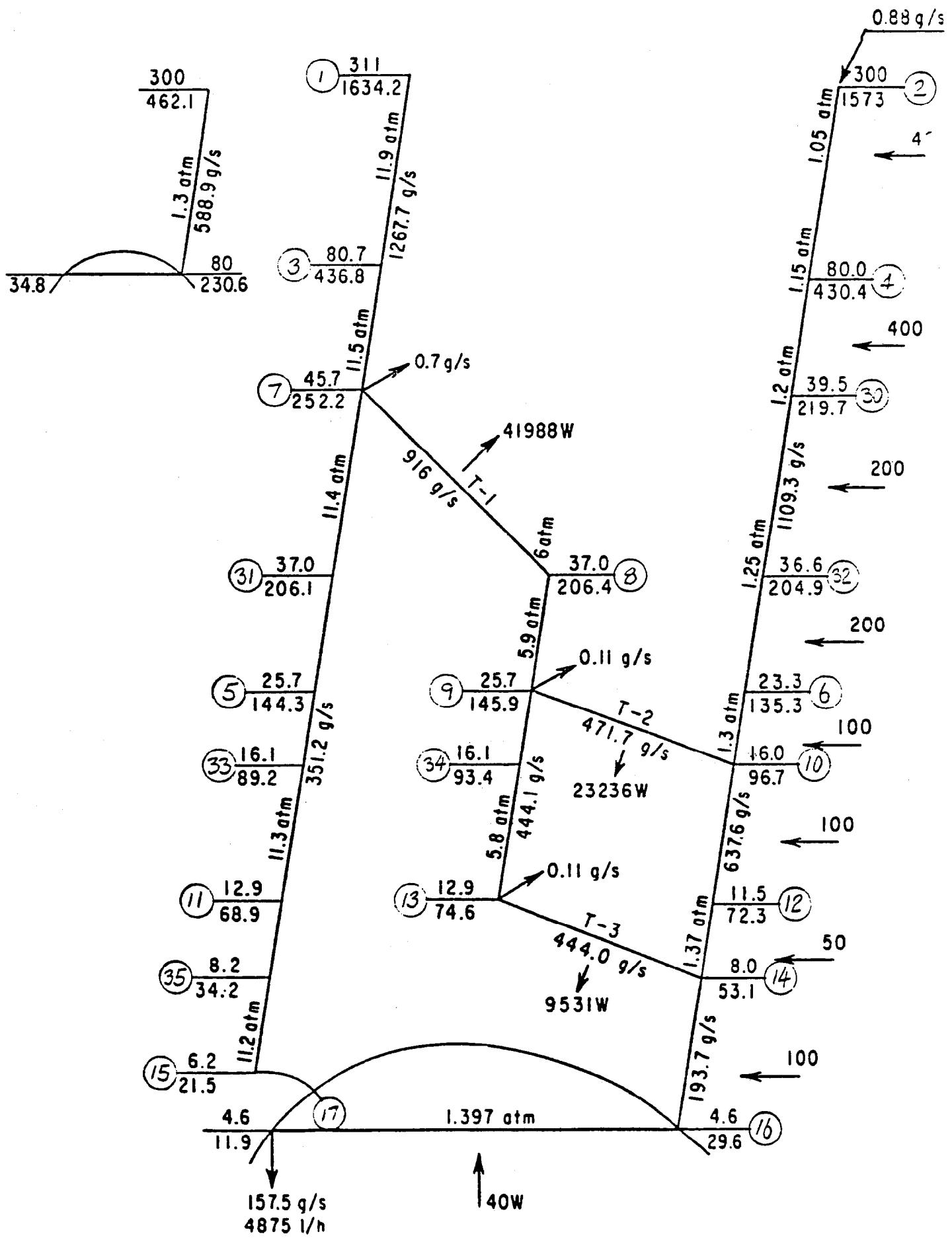


Figure 3.

CALCULATED SYSTEM DATA

FLAHT CAPACITY-LITERS/HR
4865.682

FRACTION LIQUEFIED
.453

REFRIGERATION LOADS-1/TTS
 C1 400.000 C2 400.000 C3 200.000 C4 200.000 C5 100.000 C6 100.000 C7 50.000 C8 100.000

LOAD
40.000

MASS FLOW-GM/SEC
 FT1 1266.634 FT2 1100.134 FT3 913.840 FT4 352.793 FT5 479.650 FT6 443.182 FT7 157.500 FT8 584.737

WORK-WATTS
W/CMP
2644172.13

COMPRESSOR HORSEPOWER
3544.467

CALCULATED FLUID PROPERTIES FOR SYSTEM

PRESSURE (ATM), TEMPERATURE (DEGREE K) AND ENTHALPY (J/GM)

POINT	1	2	3	4	5	6	7	8	9	10
PRESS	11.00	1.05	11.50	1.15	11.30	1.30	11.40	1.00	5.00	1.30
TEMP	311.00	300.00	290.70	280.00	25.65	23.33	45.66	27.00	29.65	16.00
ENTHALPY	1623.7	1572.4	436.3	430.4	144.2	135.3	252.2	206.4	145.0	66.6

POINT	11	12	13	14	15	16	17	17L	17V
PRESS	11.30	1.30	5.80	1.37	11.20	1.40	1.40	1.40	1.40
TEMP	12.85	11.46	12.89	8.00	6.16	4.59	4.57	4.50	4.50
ENTHALPY	69.6	72.4	74.6	53.1	21.6	20.6	21.6	11.8	20.6

POINT	30	31	32	33	34	35
PRESS	1.20	11.40	1.25	11.30	5.90	11.30
TEMP	30.50	37.00	36.65	16.10	16.10	8.22
ENTHALPY	210.8	206.0	204.0	89.1	93.2	34.3

Figure 4.

COOLING CURVE FOR HAZ

HEAT TFR TEMP DIFF	TFR P 1	TFRG 2	ENTHALPY HI PRESS	ENTHALPY LOW PRESS	ENTHALPY HI PRESS	ENTHALPY LOW PRESS	SUMMED UP
1 TC 2	1 TC 2						
6.00	.71	80.71	80.01	436.25	430.37	0.00	
7772.96	.98	79.54	78.65	430.12	423.34	0.015	.50
15545.91	1.06	78.26	77.30	423.08	416.22	17941.40	
23318.87	1.24	77.10	75.85	417.84	406.00	24620.50	
21191.82	1.41	76.01	74.70	411.71	402.28	30510.30	
39964.78	1.59	74.84	73.25	405.57	395.26	35607.05	
46637.73	1.77	73.67	71.90	399.43	388.24	40325.67	
54410.59	1.94	72.49	70.55	393.30	381.22	44520.50	
62183.54	2.12	71.32	69.00	387.14	374.20	48358.50	
60056.50	2.30	70.15	67.85	381.02	367.15	51976.60	
77720.56	2.48	69.97	66.50	374.80	360.16	56135.74	
85502.51	2.55	67.80	65.15	368.75	353.14	59166.47	
93275.47	2.83	66.63	63.80	362.61	344.12	60600.81	
101048.42	3.01	65.46	62.45	356.48	330.10	62650.50	
108821.38	3.19	64.29	61.06	350.34	322.08	65165.56	
116504.33	3.37	63.12	59.74	344.20	312.06	68524.24	
124367.29	3.55	61.95	58.30	338.07	311.64	70770.70	
132140.24	3.73	60.78	57.46	331.02	311.02	72017.01	
139613.20	3.91	59.61	55.80	325.79	304.00	74046.00	
147686.16	4.10	58.44	54.34	319.66	296.08	76887.89	
155459.11	4.28	57.27	52.66	313.52	286.64	78744.30	
163232.07	4.46	56.11	51.64	307.38	282.94	80523.30	
171005.02	4.64	54.94	50.29	301.25	275.92	82320.86	
178777.98	4.83	53.77	49.55	295.11	268.00	82872.08	
186556.93	5.01	52.61	47.40	288.97	261.88	85451.92	
194323.89	5.20	51.45	46.25	282.84	244.86	86074.32	
202097.86	5.38	50.29	44.00	276.70	247.84	86442.78	
200865.83	5.57	49.12	43.55	270.56	240.82	80862.42	
217641.76	5.75	47.96	42.20	264.43	232.80	81224.55	
225415.71	5.95	46.80	40.85	258.20	226.78	82562.85	
233188.67	6.14	45.64	39.50	252.15	210.76	83848.00	

REQUIRED UA (WATTS/K) = 93846.0
 AVERAGE LMOT (K) = 2.485
 REQUIRED NTU = 16.3

Figure 5.

COOLING CURVE FOR HX3

HEAT TFR	TEMP 1 1 TO 2	TEMP DIFF 1 TO 2	TEMP 1 HI PRESS	TEMP 2 LOW PRESS	ENTHALPY HI PRESS	ENTHALPY LOW PRESS	REQUIRED UA
54285.53	5.14	45.64	39.50	252.15	219.27	80.27	80.27
11627.90	5.75	45.67	39.41	250.61	219.27	80.27	80.27
11627.55	5.55	44.77	39.22	247.54	219.27	77.77	77.77
21710.53	5.36	44.48	39.12	246.00	217.78	77.27	77.27
2712.17	5.16	44.19	38.03	244.46	217.28	48.14	48.14
2258.80	5.07	43.90	38.03	242.02	216.70	55.50	55.50
3798.43	4.77	43.61	38.84	241.20	216.20	700.01	700.01
4341.37	4.58	43.32	38.74	238.75	215.46	81.48	81.48
4488.70	4.38	43.03	38.65	238.31	215.20	62.71	62.71
5422.33	4.10	42.74	38.55	236.77	214.81	126.27	126.27
5566.96	4.00	42.45	38.46	235.23	214.31	110.47	110.47
6531.60	3.80	42.17	38.36	233.60	213.32	122.57	122.57
7054.23	3.61	41.88	38.27	232.16	212.83	148.27	148.27
7594.86	3.41	41.59	38.17	230.62	212.33	162.66	162.66
8139.50	3.22	41.30	38.08	228.08	211.84	180.20	180.20
8682.13	3.03	41.01	37.98	227.54	211.34	1874.38	1874.38
9224.76	2.83	40.72	37.89	226.00	211.24	2150.25	2150.25
9767.40	2.64	40.43	37.79	224.47	210.85	2257.76	2257.76
10210.03	2.45	40.14	37.70	222.02	210.35	2571.22	2571.22
10652.56	2.25	39.86	37.60	221.20	209.86	2802.22	2802.22
11305.30	2.06	39.57	37.51	219.85	209.36	3054.07	3054.07
11637.93	1.87	39.28	37.41	218.31	208.86	3230.84	3230.84
12480.56	1.67	38.99	37.32	216.70	208.37	3427.30	3427.30
13222.26	1.48	38.70	37.22	215.24	207.87	3681.70	3681.70
13255.93	1.29	38.42	37.12	213.70	207.38	4374.02	4374.02
14108.46	1.10	38.13	37.02	212.16	206.89	4620.04	4620.04
14651.10	.90	37.84	36.94	210.62	206.39	5172.00	5172.00
15102.73	.71	37.56	36.84	209.09	205.89	4048.55	4048.55
15736.36	.52	37.27	36.75	207.55	205.40	4024.44	4024.44
16278.09	.33	36.98	36.65	206.01	204.50	4228.04	4228.04

REQUIRED UA (WATTS/K) = 8238.0

AVERAGE LFET (K) = 1.976

REQUIRED NTU = 1.4

Figure 6.

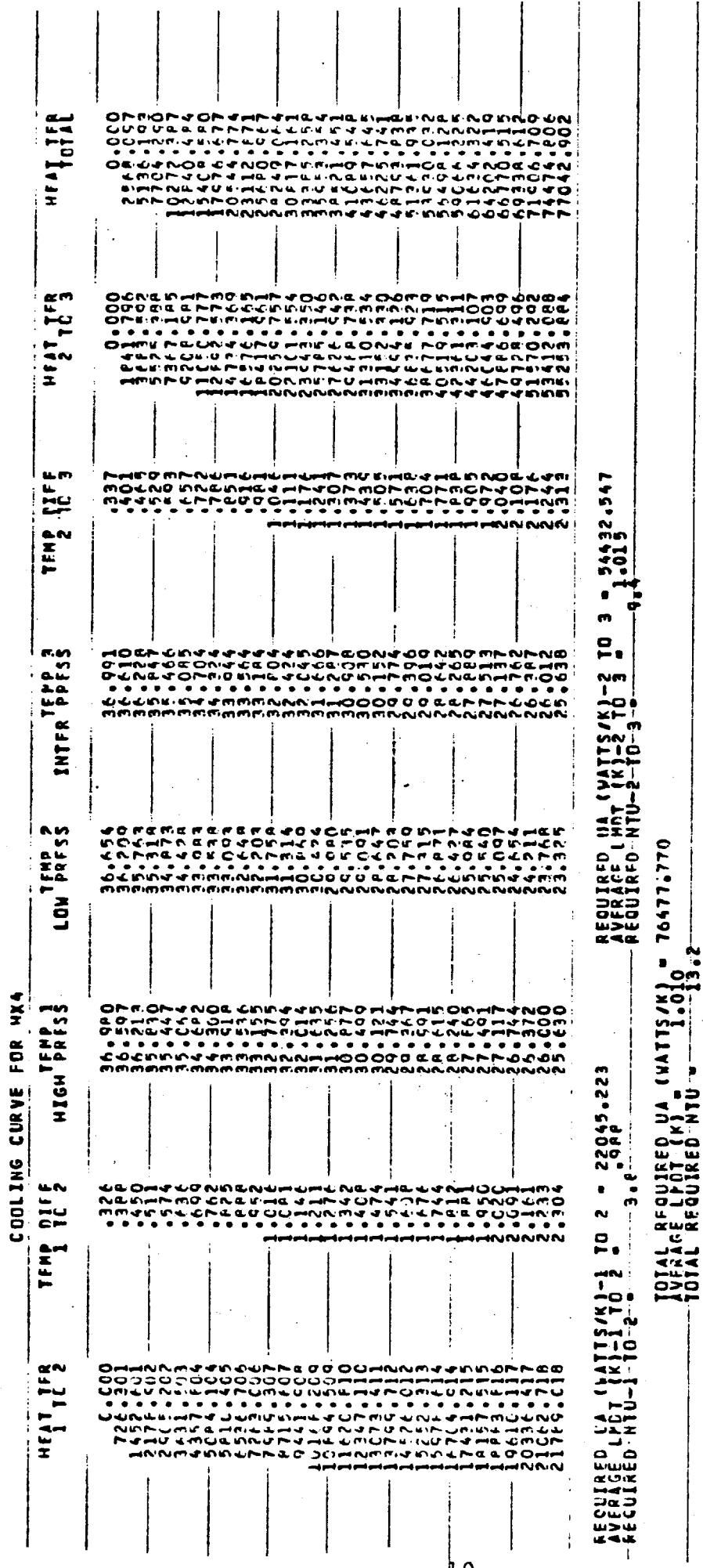


Figure 7.

COOLING CURVE FOR HX5

HEAT TFR 1 TC 2	TEMP DIFF 1 TC 2	TEMP HIGH PRESS 1	TEMP HIGH PRESS 2	LOW PRESS 1	INTER PRESS 2	TEMP DIFF 10 3	HEAT TFR 10 3
0.000	25.000	25.000	25.000	25.000	25.000	25.000	0.000
0.476	25.000	25.000	25.000	25.000	25.000	25.000	0.476
1.204	25.000	25.000	25.000	25.000	25.000	25.000	1.204
2.045	25.000	25.000	25.000	25.000	25.000	25.000	2.045
2.986	25.000	25.000	25.000	25.000	25.000	25.000	2.986
3.927	25.000	25.000	25.000	25.000	25.000	25.000	3.927
4.868	25.000	25.000	25.000	25.000	25.000	25.000	4.868
5.809	25.000	25.000	25.000	25.000	25.000	25.000	5.809
6.750	25.000	25.000	25.000	25.000	25.000	25.000	6.750
7.691	25.000	25.000	25.000	25.000	25.000	25.000	7.691
8.632	25.000	25.000	25.000	25.000	25.000	25.000	8.632
9.573	25.000	25.000	25.000	25.000	25.000	25.000	9.573
10.514	25.000	25.000	25.000	25.000	25.000	25.000	10.514
11.455	25.000	25.000	25.000	25.000	25.000	25.000	11.455
12.396	25.000	25.000	25.000	25.000	25.000	25.000	12.396
13.337	25.000	25.000	25.000	25.000	25.000	25.000	13.337
14.278	25.000	25.000	25.000	25.000	25.000	25.000	14.278
15.219	25.000	25.000	25.000	25.000	25.000	25.000	15.219
16.160	25.000	25.000	25.000	25.000	25.000	25.000	16.160
17.101	25.000	25.000	25.000	25.000	25.000	25.000	17.101
18.042	25.000	25.000	25.000	25.000	25.000	25.000	18.042
18.983	25.000	25.000	25.000	25.000	25.000	25.000	18.983
19.924	25.000	25.000	25.000	25.000	25.000	25.000	19.924
20.865	25.000	25.000	25.000	25.000	25.000	25.000	20.865
21.806	25.000	25.000	25.000	25.000	25.000	25.000	21.806
22.747	25.000	25.000	25.000	25.000	25.000	25.000	22.747
23.688	25.000	25.000	25.000	25.000	25.000	25.000	23.688
24.629	25.000	25.000	25.000	25.000	25.000	25.000	24.629
25.570	25.000	25.000	25.000	25.000	25.000	25.000	25.570
26.511	25.000	25.000	25.000	25.000	25.000	25.000	26.511
27.452	25.000	25.000	25.000	25.000	25.000	25.000	27.452
28.393	25.000	25.000	25.000	25.000	25.000	25.000	28.393
29.334	25.000	25.000	25.000	25.000	25.000	25.000	29.334
30.275	25.000	25.000	25.000	25.000	25.000	25.000	30.275
31.216	25.000	25.000	25.000	25.000	25.000	25.000	31.216
32.157	25.000	25.000	25.000	25.000	25.000	25.000	32.157
33.098	25.000	25.000	25.000	25.000	25.000	25.000	33.098
34.039	25.000	25.000	25.000	25.000	25.000	25.000	34.039
34.980	25.000	25.000	25.000	25.000	25.000	25.000	34.980
35.921	25.000	25.000	25.000	25.000	25.000	25.000	35.921
36.862	25.000	25.000	25.000	25.000	25.000	25.000	36.862
37.803	25.000	25.000	25.000	25.000	25.000	25.000	37.803
38.744	25.000	25.000	25.000	25.000	25.000	25.000	38.744
39.685	25.000	25.000	25.000	25.000	25.000	25.000	39.685
40.626	25.000	25.000	25.000	25.000	25.000	25.000	40.626
41.567	25.000	25.000	25.000	25.000	25.000	25.000	41.567
42.508	25.000	25.000	25.000	25.000	25.000	25.000	42.508
43.449	25.000	25.000	25.000	25.000	25.000	25.000	43.449
44.390	25.000	25.000	25.000	25.000	25.000	25.000	44.390
45.331	25.000	25.000	25.000	25.000	25.000	25.000	45.331
46.272	25.000	25.000	25.000	25.000	25.000	25.000	46.272
47.213	25.000	25.000	25.000	25.000	25.000	25.000	47.213
48.154	25.000	25.000	25.000	25.000	25.000	25.000	48.154
49.095	25.000	25.000	25.000	25.000	25.000	25.000	49.095
50.036	25.000	25.000	25.000	25.000	25.000	25.000	50.036
50.977	25.000	25.000	25.000	25.000	25.000	25.000	50.977
51.918	25.000	25.000	25.000	25.000	25.000	25.000	51.918
52.859	25.000	25.000	25.000	25.000	25.000	25.000	52.859
53.800	25.000	25.000	25.000	25.000	25.000	25.000	53.800
54.741	25.000	25.000	25.000	25.000	25.000	25.000	54.741
55.682	25.000	25.000	25.000	25.000	25.000	25.000	55.682
56.623	25.000	25.000	25.000	25.000	25.000	25.000	56.623
57.564	25.000	25.000	25.000	25.000	25.000	25.000	57.564
58.505	25.000	25.000	25.000	25.000	25.000	25.000	58.505
59.446	25.000	25.000	25.000	25.000	25.000	25.000	59.446
60.387	25.000	25.000	25.000	25.000	25.000	25.000	60.387
61.328	25.000	25.000	25.000	25.000	25.000	25.000	61.328
62.269	25.000	25.000	25.000	25.000	25.000	25.000	62.269
63.210	25.000	25.000	25.000	25.000	25.000	25.000	63.210
64.151	25.000	25.000	25.000	25.000	25.000	25.000	64.151
65.092	25.000	25.000	25.000	25.000	25.000	25.000	65.092
66.033	25.000	25.000	25.000	25.000	25.000	25.000	66.033
66.974	25.000	25.000	25.000	25.000	25.000	25.000	66.974
67.915	25.000	25.000	25.000	25.000	25.000	25.000	67.915
68.856	25.000	25.000	25.000	25.000	25.000	25.000	68.856
69.797	25.000	25.000	25.000	25.000	25.000	25.000	69.797
70.738	25.000	25.000	25.000	25.000	25.000	25.000	70.738
71.679	25.000	25.000	25.000	25.000	25.000	25.000	71.679
72.620	25.000	25.000	25.000	25.000	25.000	25.000	72.620
73.561	25.000	25.000	25.000	25.000	25.000	25.000	73.561
74.502	25.000	25.000	25.000	25.000	25.000	25.000	74.502
75.443	25.000	25.000	25.000	25.000	25.000	25.000	75.443
76.384	25.000	25.000	25.000	25.000	25.000	25.000	76.384
77.325	25.000	25.000	25.000	25.000	25.000	25.000	77.325
78.266	25.000	25.000	25.000	25.000	25.000	25.000	78.266
79.207	25.000	25.000	25.000	25.000	25.000	25.000	79.207
80.148	25.000	25.000	25.000	25.000	25.000	25.000	80.148
81.089	25.000	25.000	25.000	25.000	25.000	25.000	81.089
82.030	25.000	25.000	25.000	25.000	25.000	25.000	82.030
82.971	25.000	25.000	25.000	25.000	25.000	25.000	82.971
83.912	25.000	25.000	25.000	25.000	25.000	25.000	83.912
84.853	25.000	25.000	25.000	25.000	25.000	25.000	84.853
85.794	25.000	25.000	25.000	25.000	25.000	25.000	85.794
86.735	25.000	25.000	25.000	25.000	25.000	25.000	86.735
87.676	25.000	25.000	25.000	25.000	25.000	25.000	87.676
88.617	25.000	25.000	25.000	25.000	25.000	25.000	88.617
89.558	25.000	25.000	25.000	25.000	25.000	25.000	89.558
90.500	25.000	25.000	25.000	25.000	25.000	25.000	90.500
91.441	25.000	25.000	25.000	25.000	25.000	25.000	91.441
92.382	25.000	25.000	25.000	25.000	25.000	25.000	92.382
93.323	25.000	25.000	25.000	25.000	25.000	25.000	93.323
94.264	25.000	25.000	25.000	25.000	25.000	25.000	94.264
95.205	25.000	25.000	25.000	25.000	25.000	25.000	95.205
96.146	25.000	25.000	25.000	25.000	25.000	25.000	96.146
97.087	25.000	25.000	25.000	25.000	25.000	25.000	97.087
97.028	25.000	25.000	25.000	25.000	25.000	25.000	97.028
97.969	25.000	25.000	25.000	25.000	25.000	25.000	97.969
98.910	25.000	25.000	25.000	25.000	25.000	25.000	98.910
99.851	25.000	25.000	25.000	25.000	25.000	25.000	99.851
100.792	25.000	25.000	25.000	25.000	25.000	25.000	100.792

REQUIRED UA (WATTS/K) -1 TO 2 = 31226.740
 AVERAGE LNUT (K) -2 TO 3 = .625
 REQUIRED LNUT -1 TO 2 = .53

REQUIRED LNUT -2 TO 3 = .641
 REQUIRED NTU -2 TO 3 = .642

TOTAL REQUIRED UA (WATTS/K) = .634
 AVERAGE LNUT (K) = .634
 REQUIRED NTU = .634

TOTAL REQUIRED NTU = .634

Figure 8.

CORRECTING CURVE FOR HX6

REQUIRED UA (WATTS/K)-2 TO 3 = 16367.162
AVERAGED LNT (W/K)-2 = 6491

Figure 9.

COOLING CURVE FOR HX7

HEAT TFR 1 TC 2	TEMP DIFF 1 TO 2	TEMP 1 HI PRESS	TEMP 2 LOW PRESS	ENTHALPY HI PRESS	ENTHALPY LOW PRESS	SUMMED UA
0.00	1.45	12.92	11.48	68.98	72.36	0.00
407.24	1.39	12.75	11.36	67.82	71.72	297.82
815.88	1.33	12.57	11.24	66.66	71.07	587.65
1222.82	1.28	12.40	11.12	65.51	70.43	802.27
1631.76	1.22	12.22	11.00	64.35	69.79	1227.00
2036.70	1.17	12.05	10.89	63.10	68.15	1548.44
2447.54	1.12	11.88	10.77	62.84	67.51	3024.54
2855.50	1.06	11.71	10.65	62.58	67.87	2202.14
3263.53	1.01	11.54	10.53	62.32	67.23	2404.04
3671.47	.96	11.37	10.42	62.07	66.58	2112.84
4079.41	.91	11.21	10.30	61.81	65.94	2551.24
4487.35	.85	11.04	10.18	61.56	65.30	4014.76
4895.29	.81	10.87	10.07	61.30	64.66	4505.51
5303.23	.76	10.71	9.95	61.04	64.02	5025.00
5711.17	.72	10.55	9.83	60.79	63.38	5778.82
6119.11	.67	10.39	9.72	60.53	62.73	6166.70
6527.05	.63	10.23	9.60	60.27	62.09	6202.72
6934.99	.59	10.08	9.49	60.02	61.45	7450.45
7342.93	.56	9.93	9.37	59.76	60.81	8150.74
7750.87	.52	9.78	9.26	59.51	60.17	8026.10
8158.81	.49	9.63	9.14	59.25	59.83	8731.20
8566.76	.46	9.49	9.03	58.99	58.80	10597.02
8974.70	.44	9.35	8.91	58.74	58.24	11405.97
9382.64	.41	9.21	8.80	58.48	57.60	12480.64
9790.58	.38	9.07	8.68	58.22	56.96	13484.57
10198.52	.36	8.93	8.57	58.07	56.32	14572.50
10606.46	.34	8.79	8.45	57.91	55.88	15723.18
11014.40	.31	8.65	8.34	57.75	55.84	16008.46
11422.34	.29	8.51	8.22	57.60	54.39	16247.02
11830.28	.26	8.37	8.12	57.44	53.75	16954.27
12238.22	.22	8.22	8.00	54.29	53.11	21560.23

REQUIRED UA (WATTS/K) = 21565.8
 AVERAGE LMTT (K) = 567
 REQUIRED PTU = 6.1

Figure 10.

COOLING CURVE FOR HX

HEAT T ₂	T ₂ P	T ₁ P ₁	T ₁ P ₂	TEMP 1 HI PRESS	TEMP 2 LOW PRESS	F _H THALPY HI PRESS	F _L THALPY LOW PRESS	SUMMED '1A
1.00	.20	6.22	8.01	34.29	53.11	6.70		
1.49	.28	8.16	7.98	33.86	52.32	620.01		
2.09	.35	8.11	7.74	32.44	51.54	1084.48		
4.49	.03	8.05	7.61	32.01	50.76	1455.64		
5.98	.70	7.00	7.47	32.56	48.98	1744.00		
7.48	.38	7.94	7.24	32.16	48.19	2022.55		
8.98	.05	7.98	7.21	31.74	48.41	2260.05		
1.047	.72	7.92	7.67	31.32	47.63	2470.86		
1.107	.40	7.76	6.94	30.99	46.84	2671.06		
1.357	.08	7.70	6.81	30.47	45.06	2846.24		
1.406	.75	7.64	6.68	30.04	45.28	3000.44		
1.646	.43	7.58	6.56	29.62	44.49	3150.54		
1.796	.10	7.52	6.43	29.20	43.71	3301.77		
1.945	.78	7.45	6.20	28.77	42.93	3434.08		
2.095	.45	7.21	6.10	28.35	42.14	3561.77		
2.245	.12	7.27	6.06	27.92	41.36	3682.59		
2.394	.80	7.22	7.26	27.50	40.58	3708.17		
2.544	.48	7.37	7.00	27.07	40.76	3800.21		
2.694	.16	7.42	7.13	26.65	40.01	4014.20		
2.842	.83	7.47	7.06	26.22	39.23	4110.01		
2.992	.51	7.51	6.80	25.80	37.44	4220.56		
3.142	.18	7.54	6.92	25.37	36.66	4318.55		
3.292	.86	7.58	6.84	24.95	35.87	4414.50		
3.442	.53	7.60	6.77	24.53	35.00	4508.77		
3.592	.21	7.62	6.60	24.10	34.21	4601.56		
3.741	.88	7.64	6.51	23.68	33.32	4602.34		
3.891	.56	7.65	6.53	23.25	32.54	4794.51		
4.041	.23	7.65	6.45	22.83	31.76	4875.67		
4.190	.01	7.64	6.37	22.41	31.17	4984.67		
4.340	.58	7.62	6.28	21.98	30.38	5058.67		
4.490	.26	7.59	6.19	21.56	29.61	5151.00		

REQUIRED UA (WATTS/K) = 5151.9
 AVERAGE LNCT (K) = .872
 REQUIRED HTL = 3.8

Figure 11.

TURBINE SPECIFICATIONS

TURBINE T1

ADIABATIC EFFICIENCY	.835
MASS FLOW-GM/SEC	913.840
PRESSURE RATIO	1.900
WORK-WATTS	41842.975
	INLET OUTLET
PRESSURE-ATM	11.400 6.000
TEMPERATURE-K	45.655 37.000
ENTHALPY-J/GM	252.152 205.364
ENTROPY-J/GM-K	16.532 16.780
SPECIFIC HEAT,CP-J/GM-K	5.304 5.285
SPECIFIC HEAT RATIO,CP/CV	1.692 1.600
DENSITY-GM/CC	1.1F7E-02 7.804E-03
VISCOSITY-GM/CM-SEC	6.226E-05 5.400E-05

Figure 12.

TURBINE SPECIFICATIONS

TURBINE T2

ADIABATIC EFFICIENCY	.820
MASS FLOW-GM/SEC	470.659
PRESSURE RATIO	4.538
WORK-WATTS	23185.772
	INLET OUTLET
PRESSURE-ATM	5.000 1.200
TEMPERATURE-K	25.650 16.000
ENTHALPY-J/GM	145.901 96.639
ENTROPY-J/GM-K	14.862 15.580
SPECIFIC HEAT,CP-J/GM-K	5.390 5.307
SPECIFIC HEAT RATIO,CP/CV	1.722 1.702
DENSITY-GM/CC	1.175E-02 3.003E-03
VISCOSITY-GM/CM-SEC	4.396E-05 3.113E-05

TURBINE SPECIFICATIONS

TURBINE T3

ADIABATIC EFFICIENCY	.820
MASS FLOW-GM/SEC	443.182
PRESSURE RATIO	4.234
WORK-WATTS	9538.468
	INLET OUTLET
PRESSURE-ATM	5.800 1.270
TEMPERATURE-K	12.891 9.000
ENTHALPY-J/GM	74.634 53.111
ENTROPY-J/GM-K	11.032 11.696
SPECIFIC HEAT,CP-J/GM-K	6.036 5.722
SPECIFIC HEAT RATIO,CP/CV	1.941 1.940
DENSITY-GM/CC	2.370E-02 9.007E-03
VISCOSITY-GM/CM-SEC	2.999E-05 1.973E-05

Figure 13.

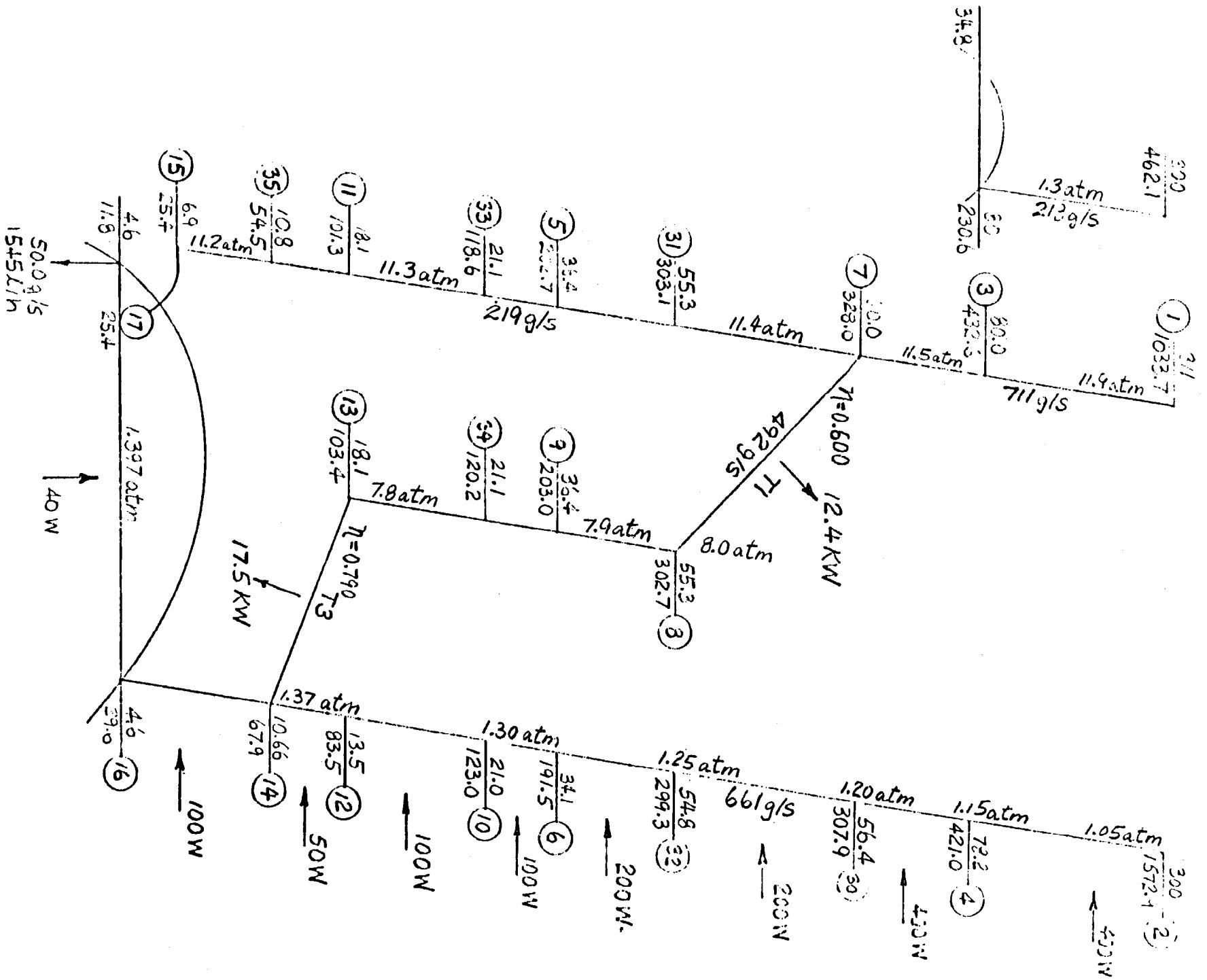


Figure 14.

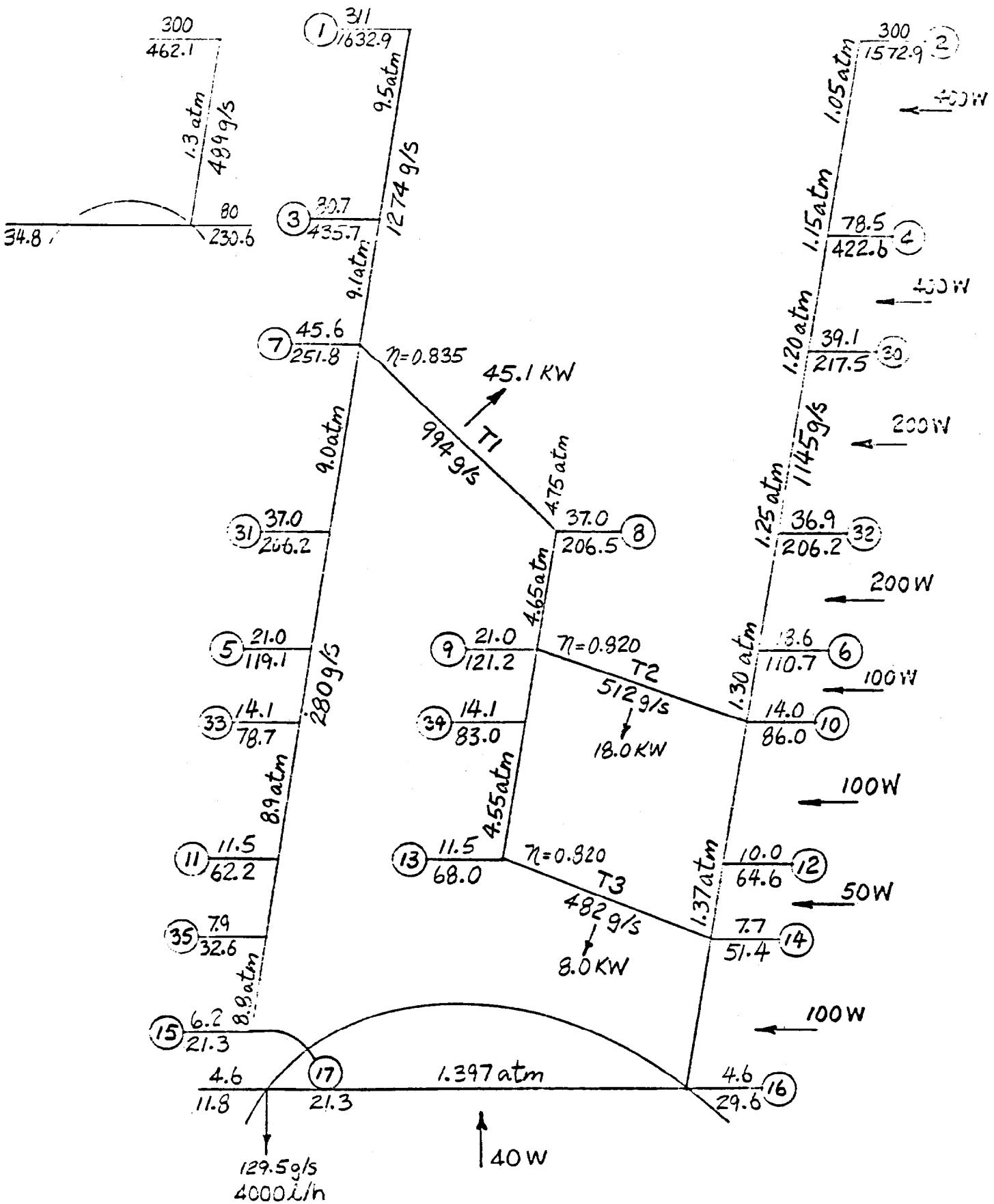


Figure 15.

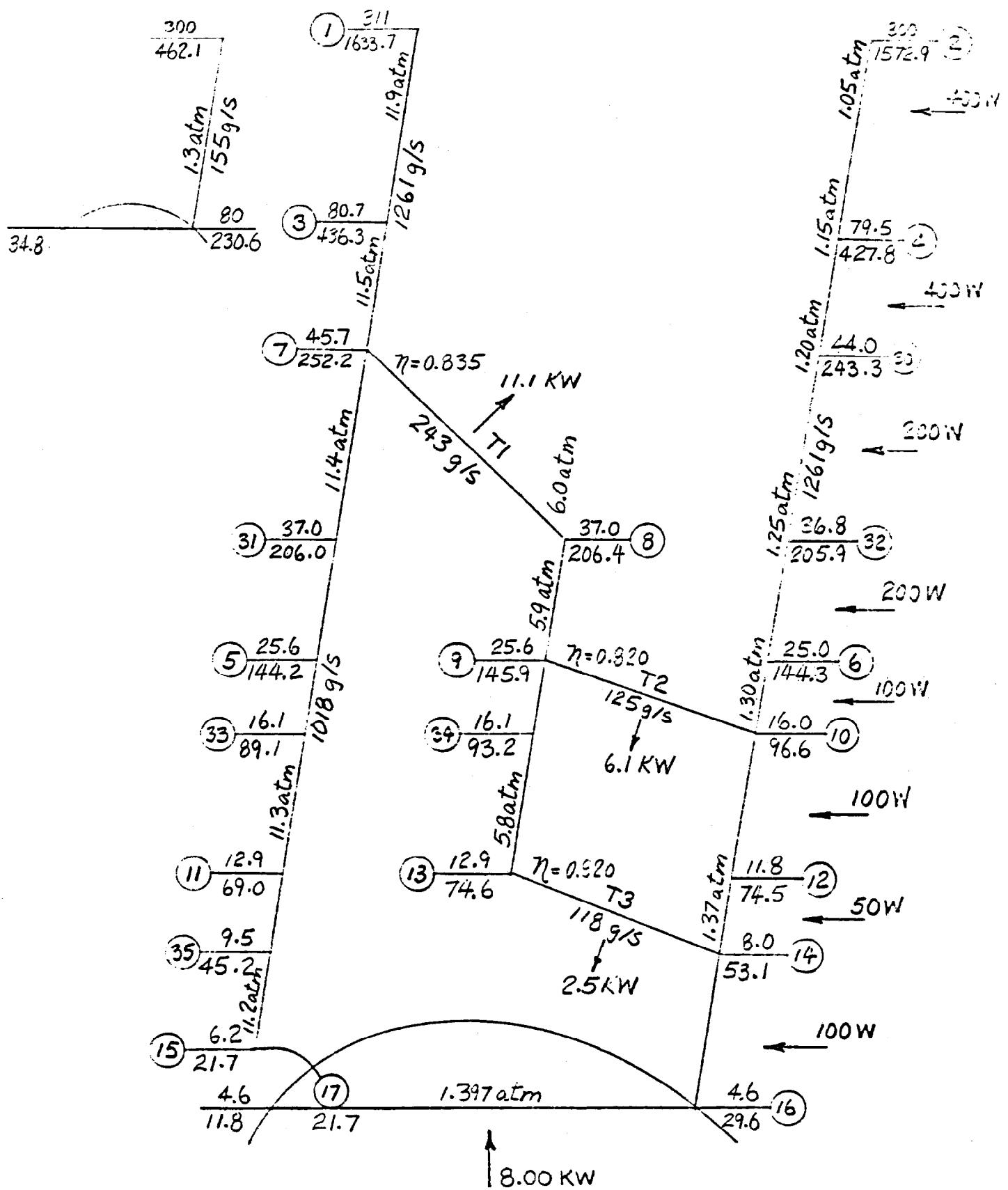


Figure 16.